

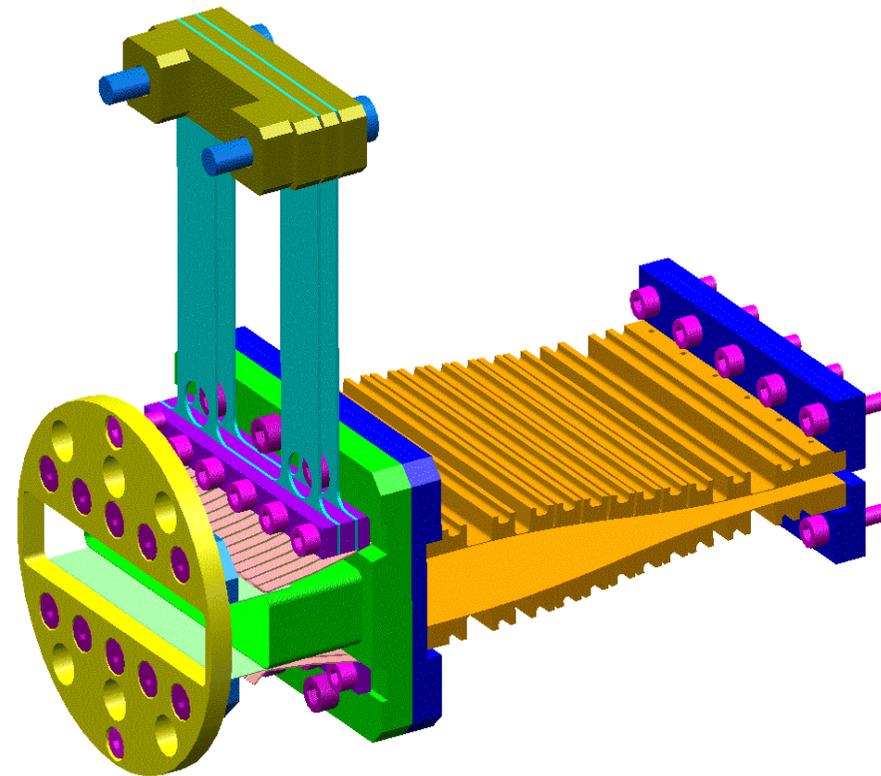
Flexible bearings for high precision mechanisms in accelerator facilities

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CSEM

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PSI

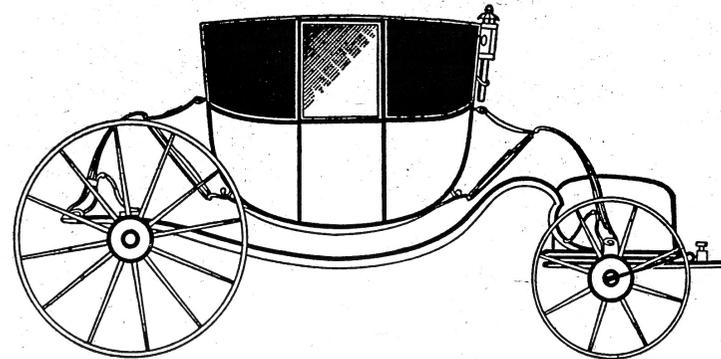


Presentation outline

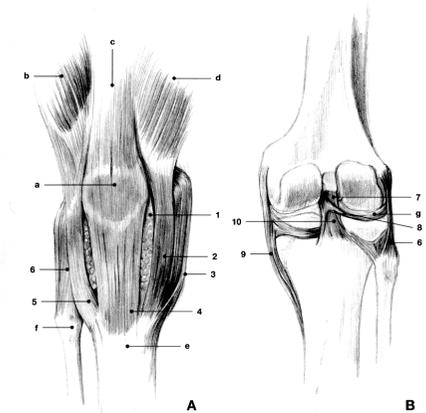
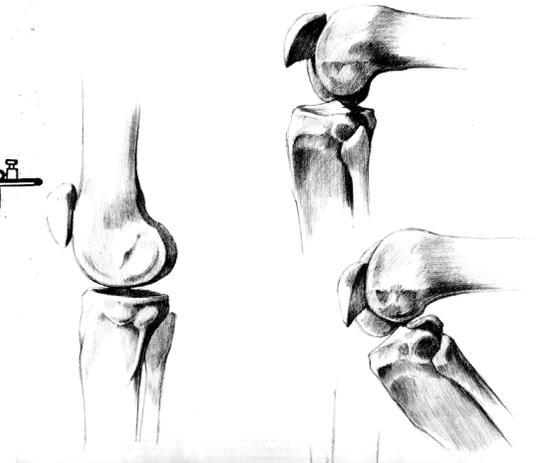
- Introduction
- Flexible bearings design methodology
 - Stroke
 - Parasitic movements
 - Restoring force
 - High precision mechanisms examples (CSEM)
- Compliant mechanisms in accelerator facilities
 - Why compliant mechanisms
 - Examples of use
- Conclusion

Introduction

- Old approach
- New needs
 - extreme precision
 - cleanliness
 - hostile environments:
vacuum, cryogenic, vibrations
- New technologies
 - Electro-discharge machining
 - Silicon technologies, MEMs



Coach with leaf springs 1820

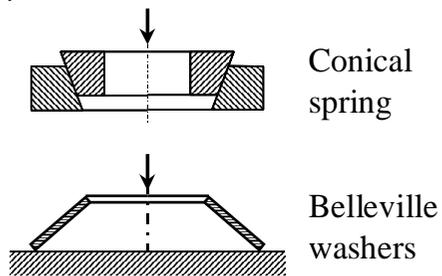


Elementary Articulations

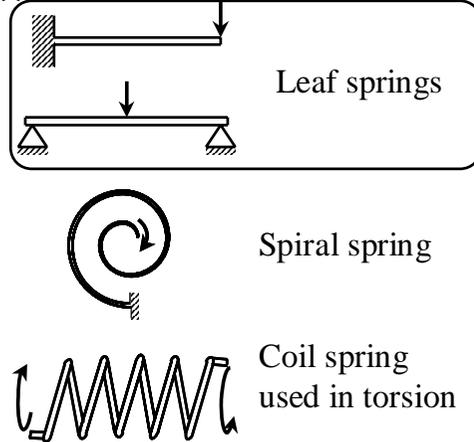
Normal Stress

Shear Stress

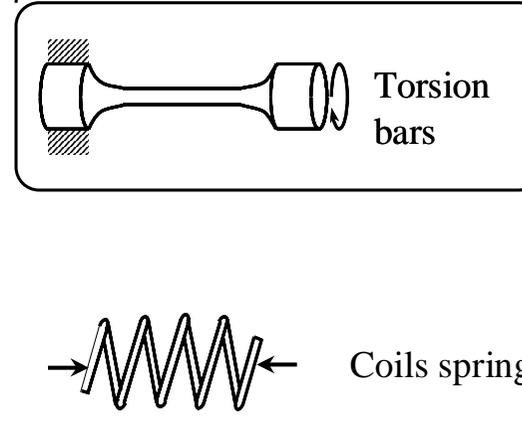
Tension and Compression



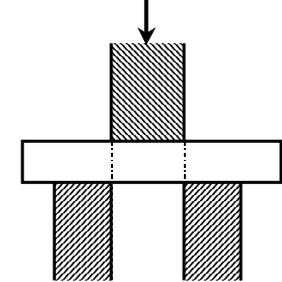
Bending



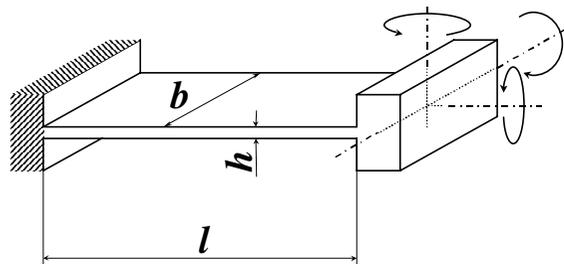
Torsion



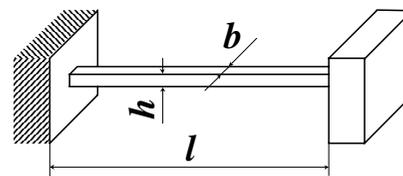
Simple Shear



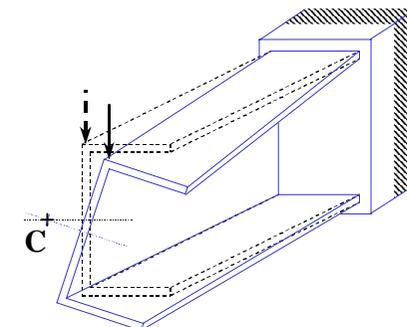
leaf spring



flexible rod



torsion bar



Flexible bearings

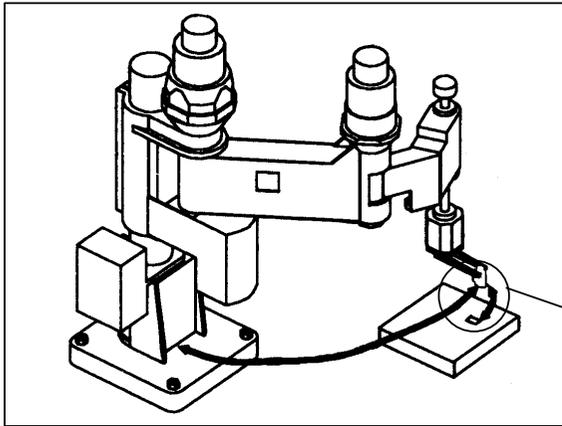
Advantages

- High precision
- No friction
- No hysteresis
- No wear
- No lubrication
- No risk of jamming
- No backlash
- Monolithic manufacturing (“design for no assembly”)
- Main sources of errors are systematic => simple control laws can be used
- Small cost

Limitations

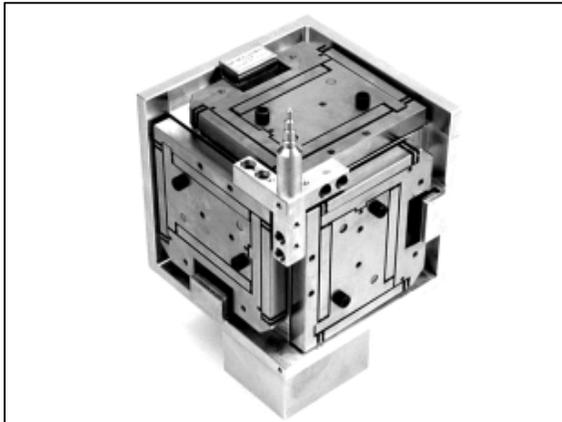
- Limited stroke
- Limited load capacity
- Restoring force
- Complex kinematics

Categorisation



Machines
Robots

High precision
mechanisms

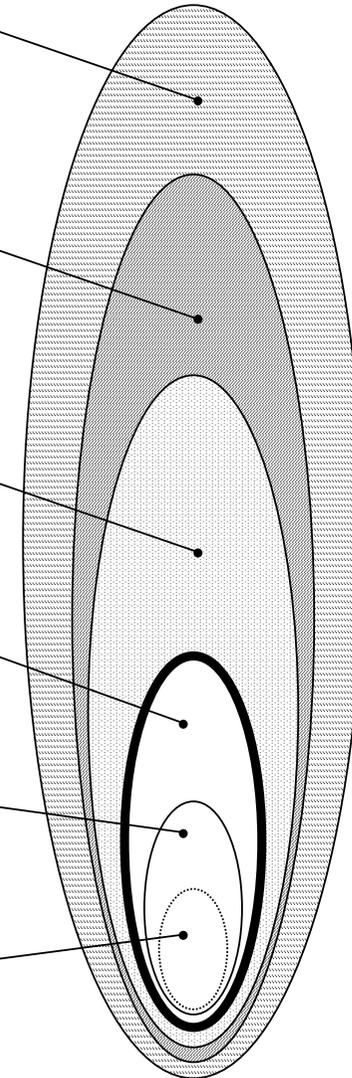
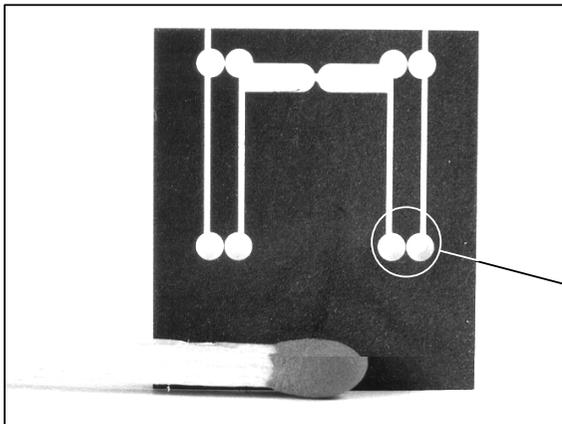


Mechanical structures

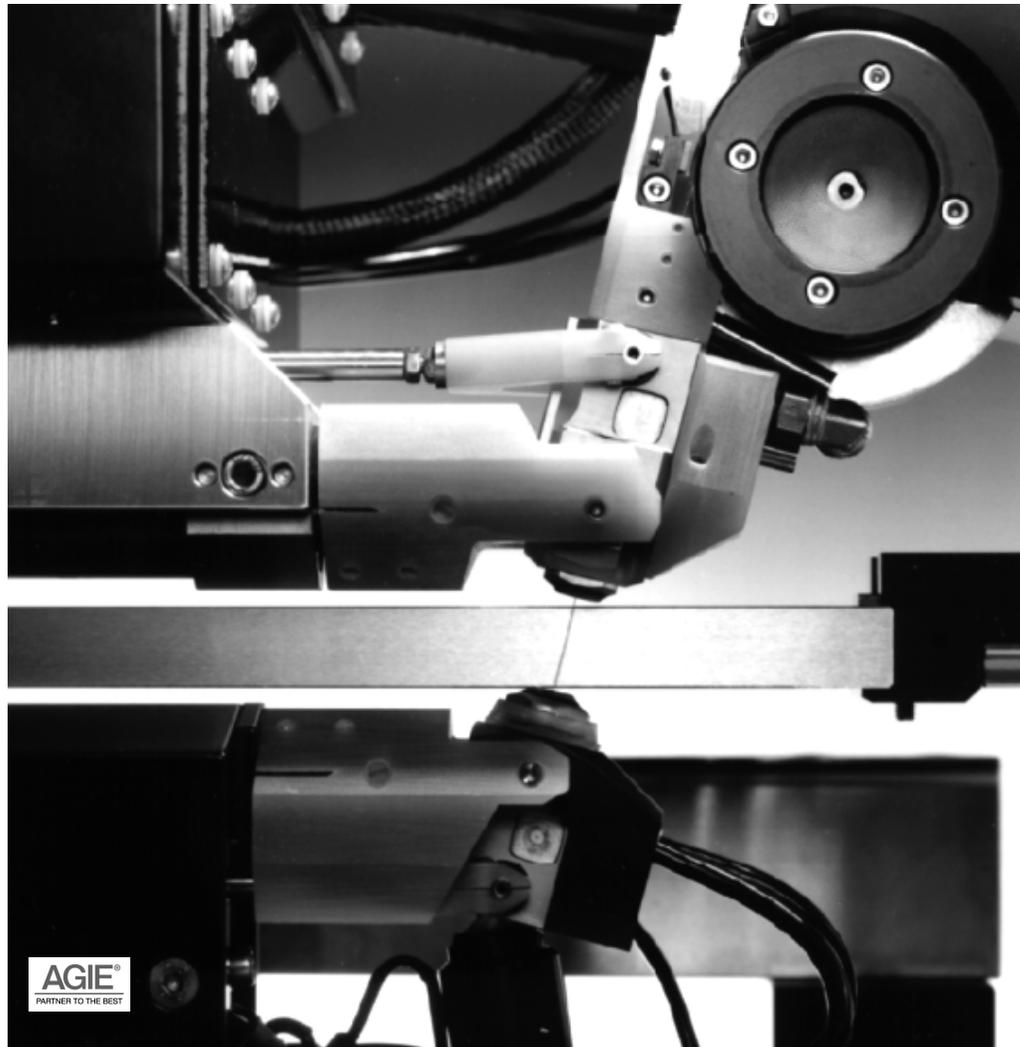
Flexible structures

Flexible bearings

Elementary
flexible articulations

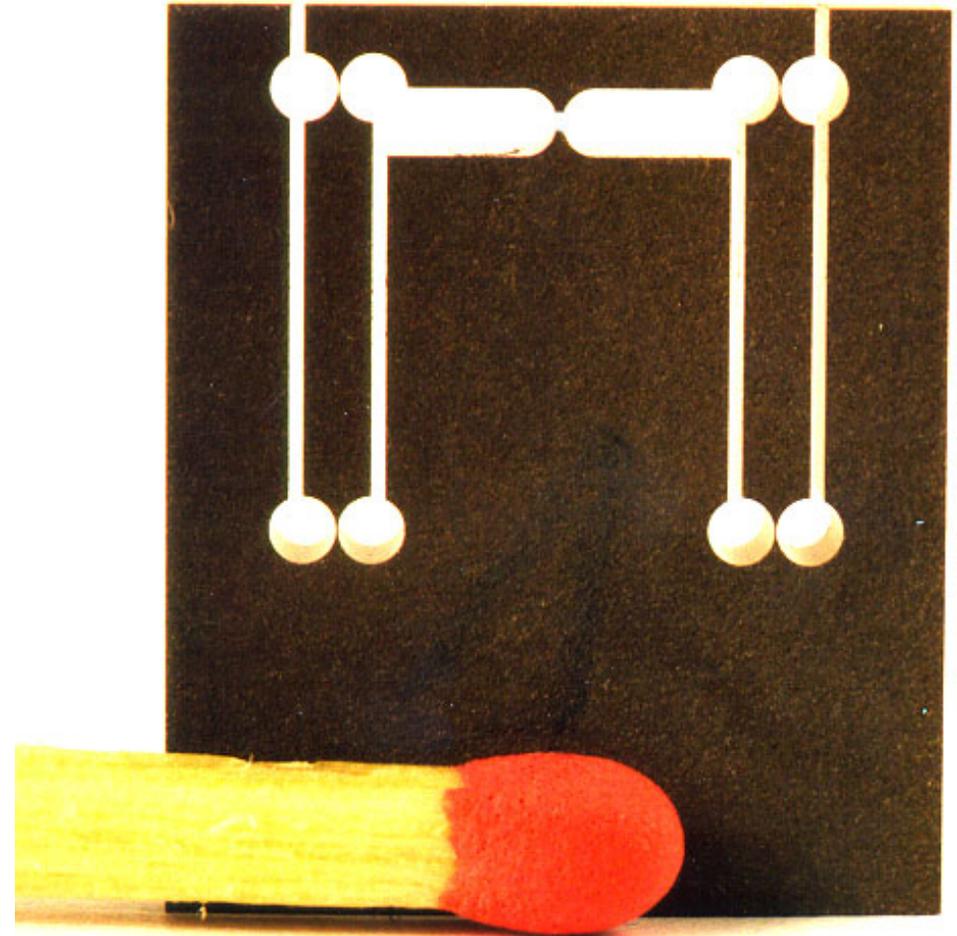
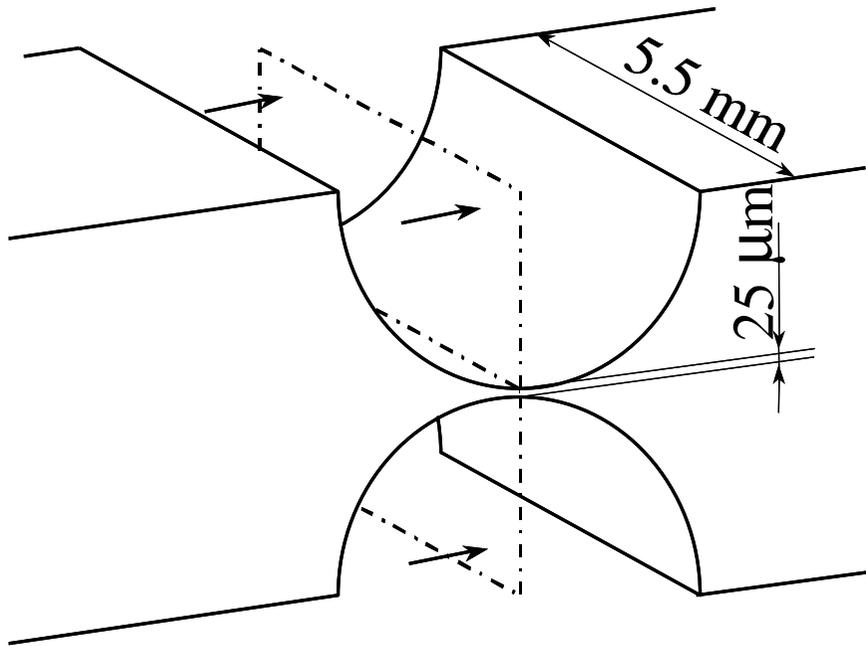


Wire electro-discharge machining



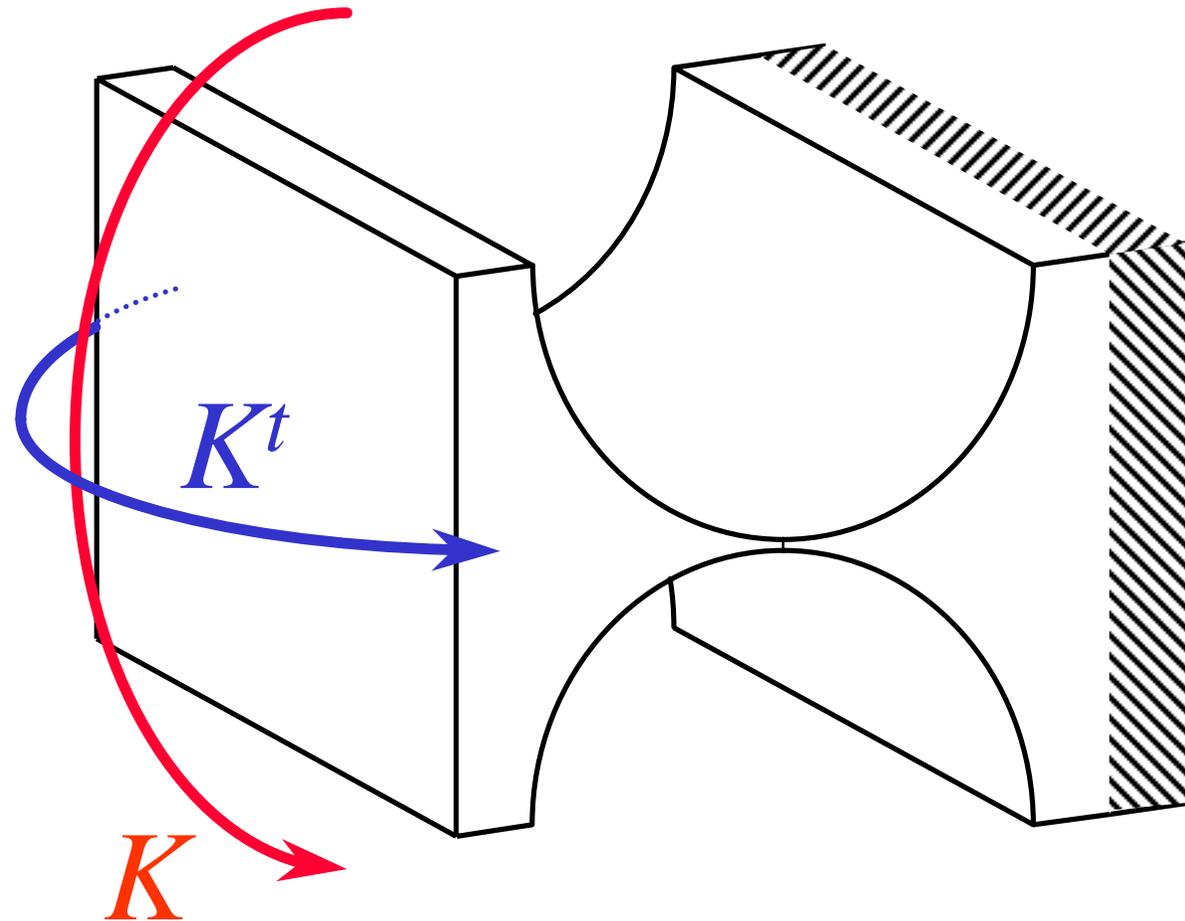
- Very small machining forces
- Insensitivity to hardness
- High aspect ratios
- High precision
- Monolithic machining

High Aspect Ratios

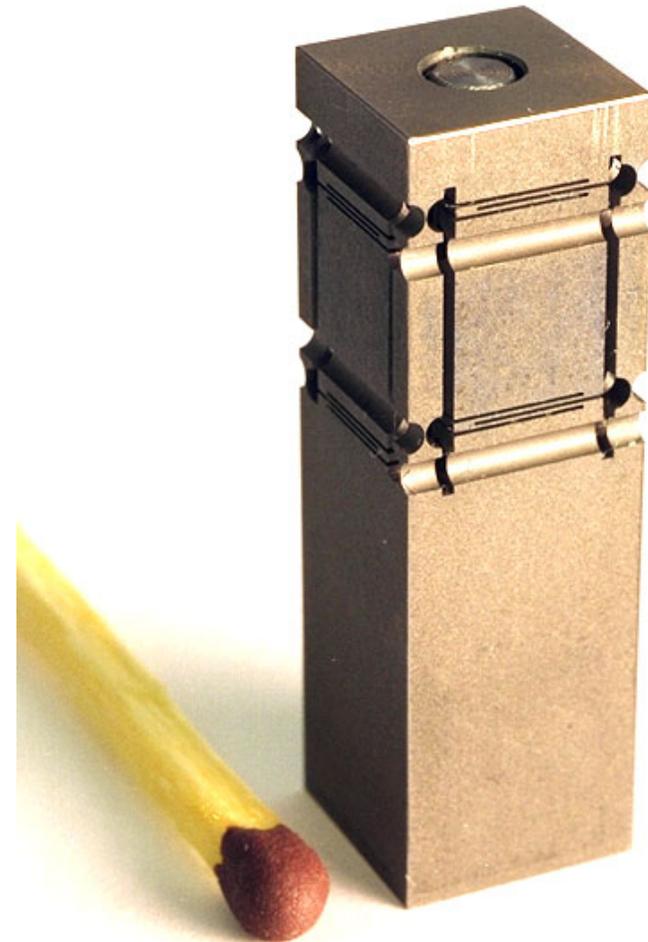
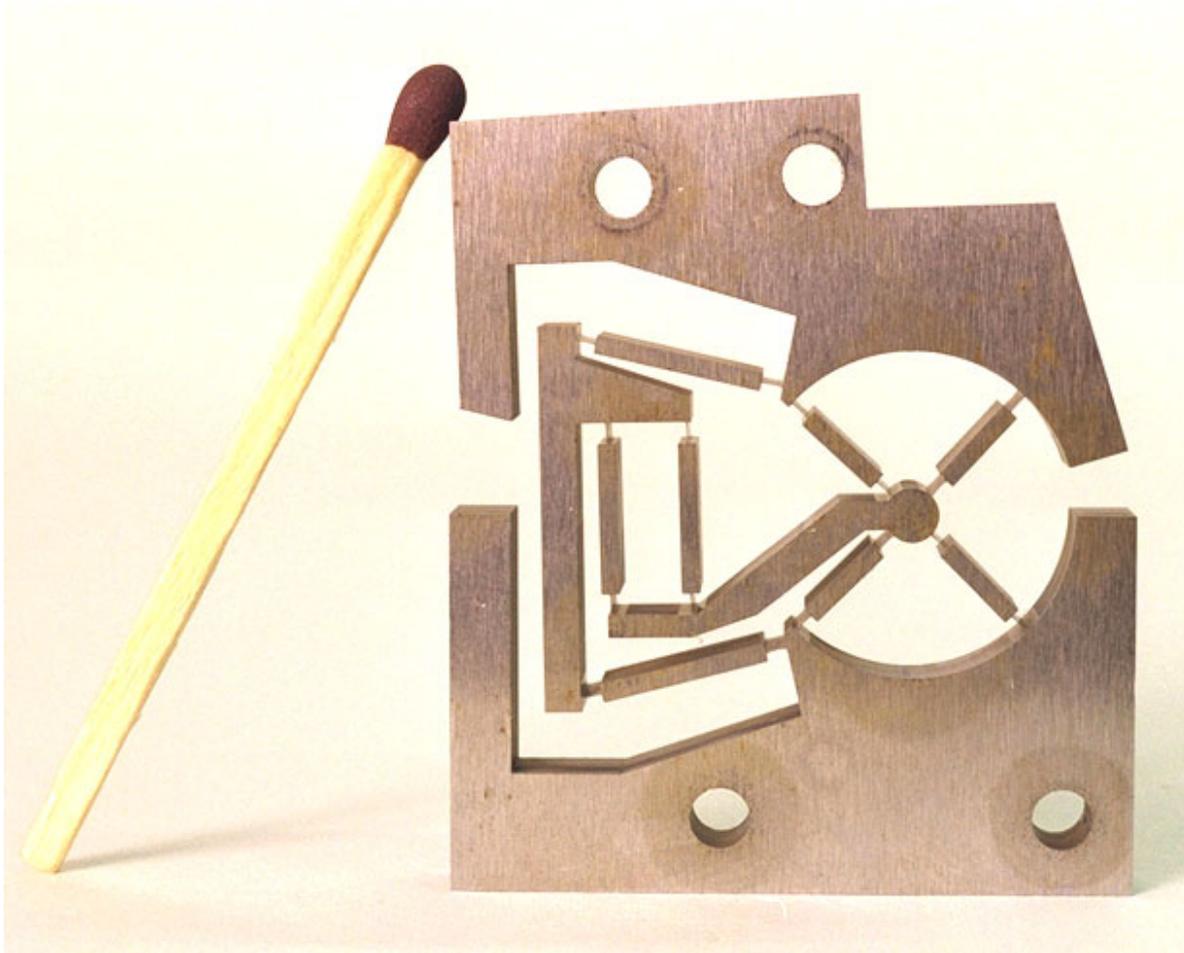


High Stiffness Ratios

$$\frac{K^t}{K} > 20'000$$



Monolithic manufacturing of complex structures

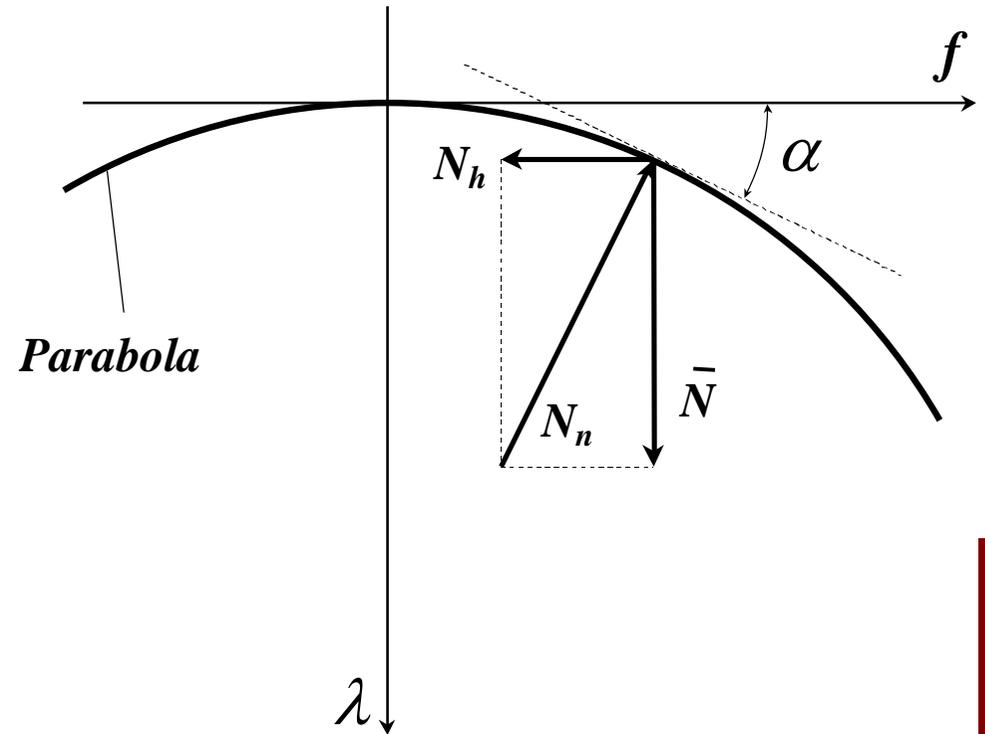
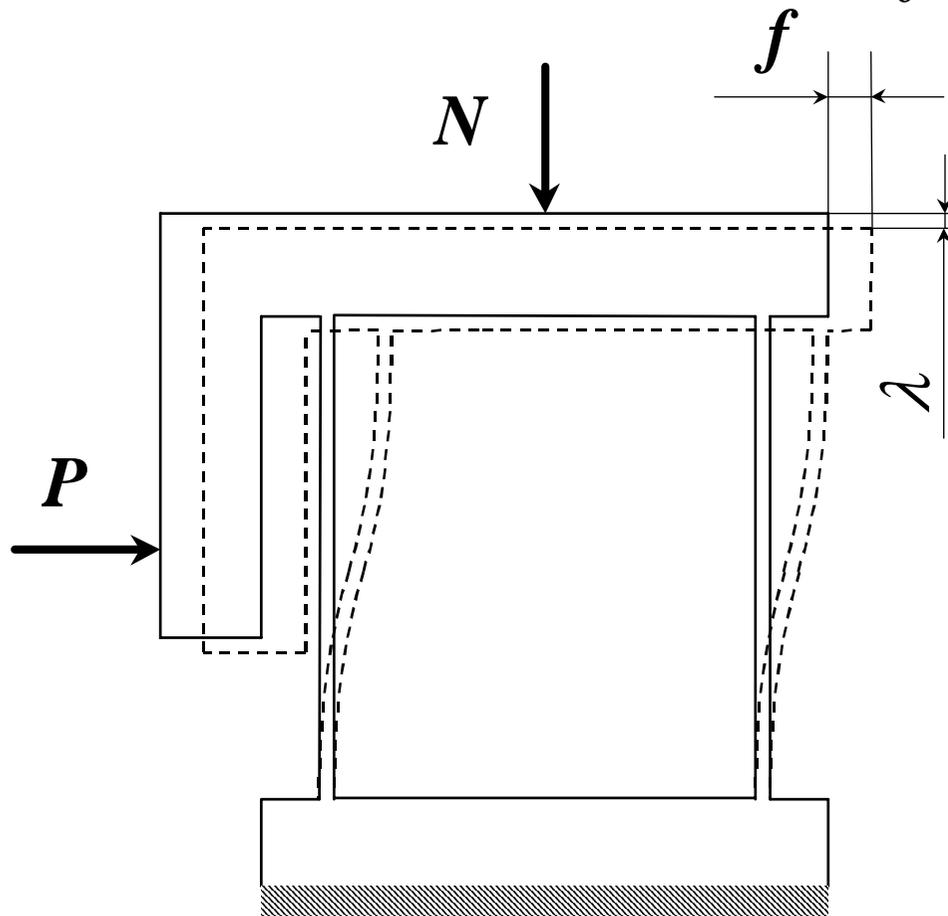


R. Clavel, S. Henein

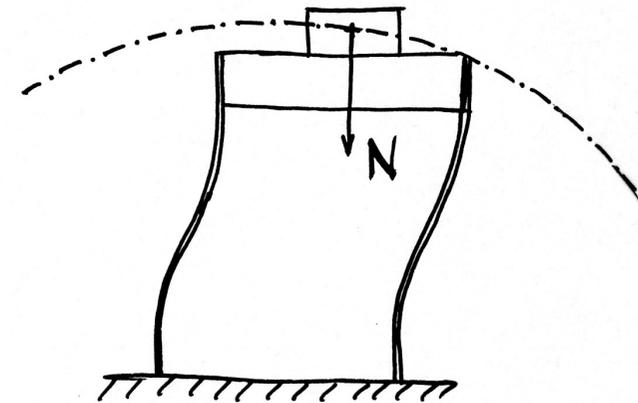
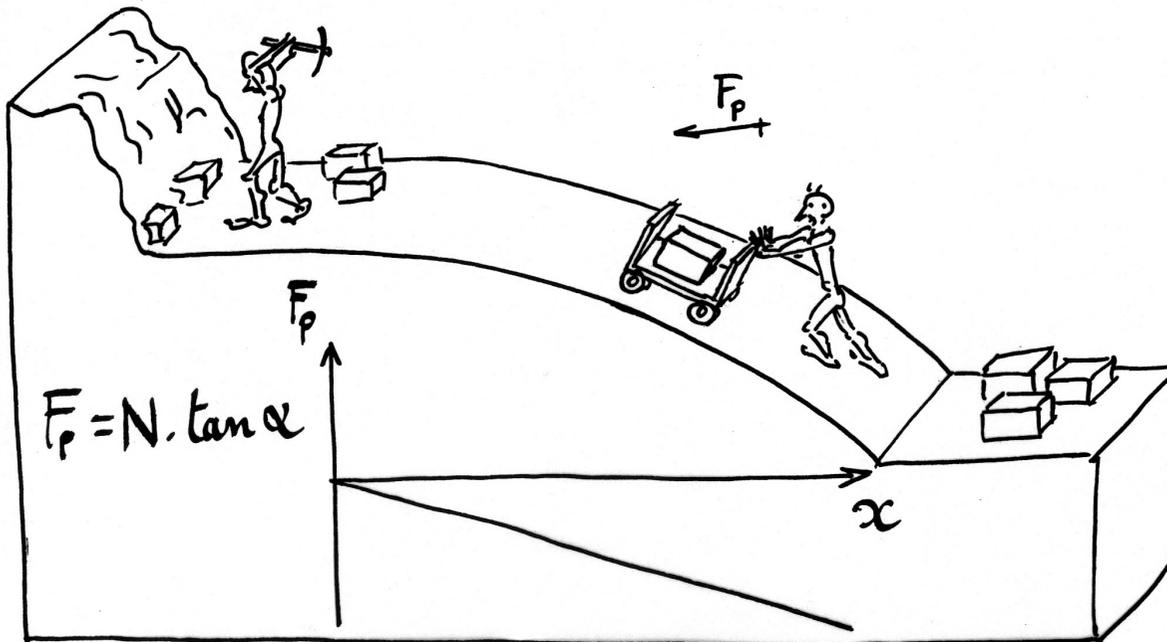
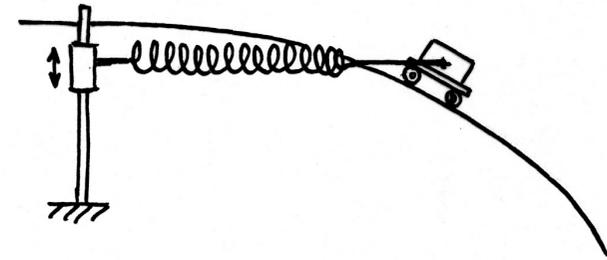
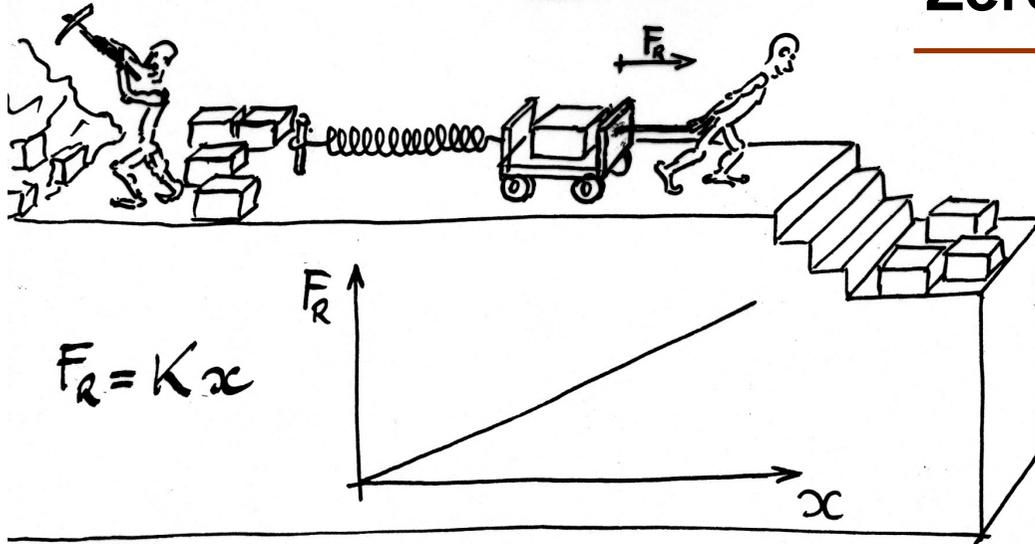


Parallel spring stage

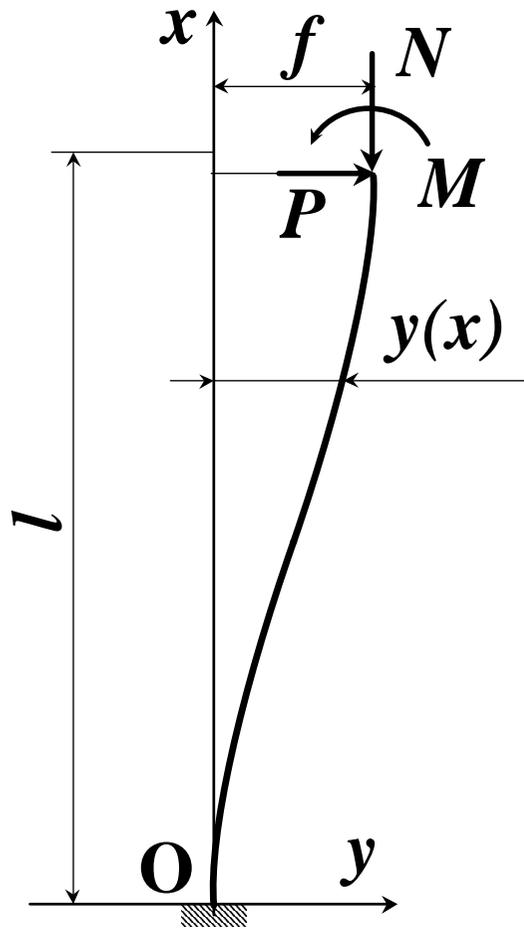
The stiffness $K = \frac{P}{f}$ depends of the load N



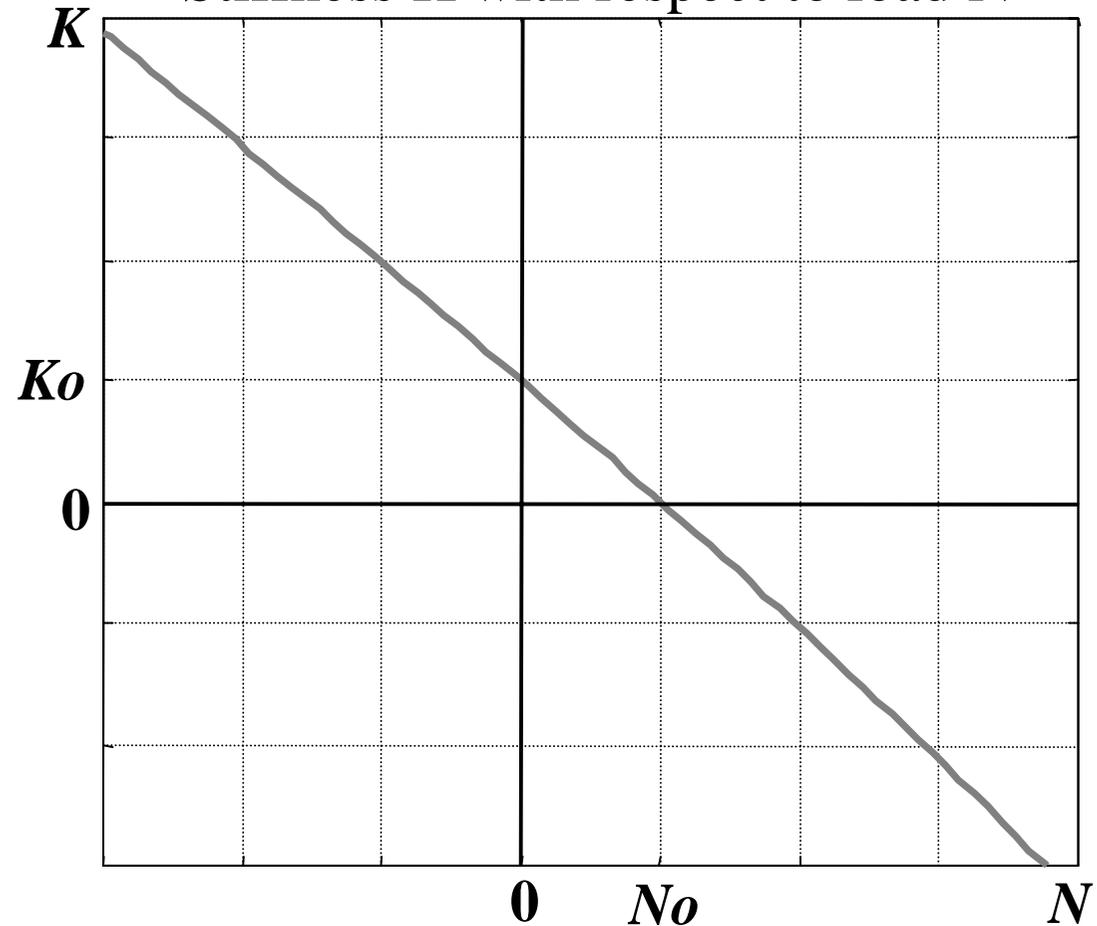
Zero stiffness flexible bearing



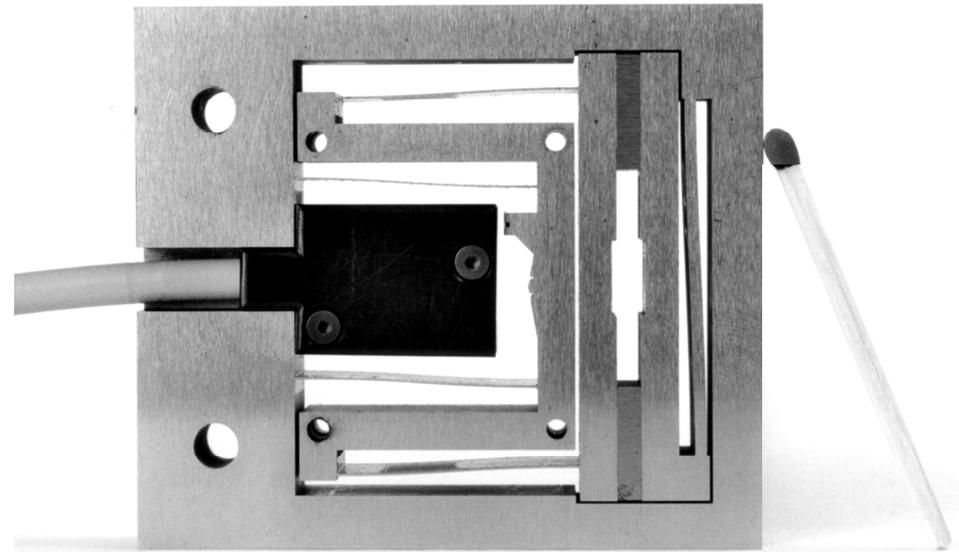
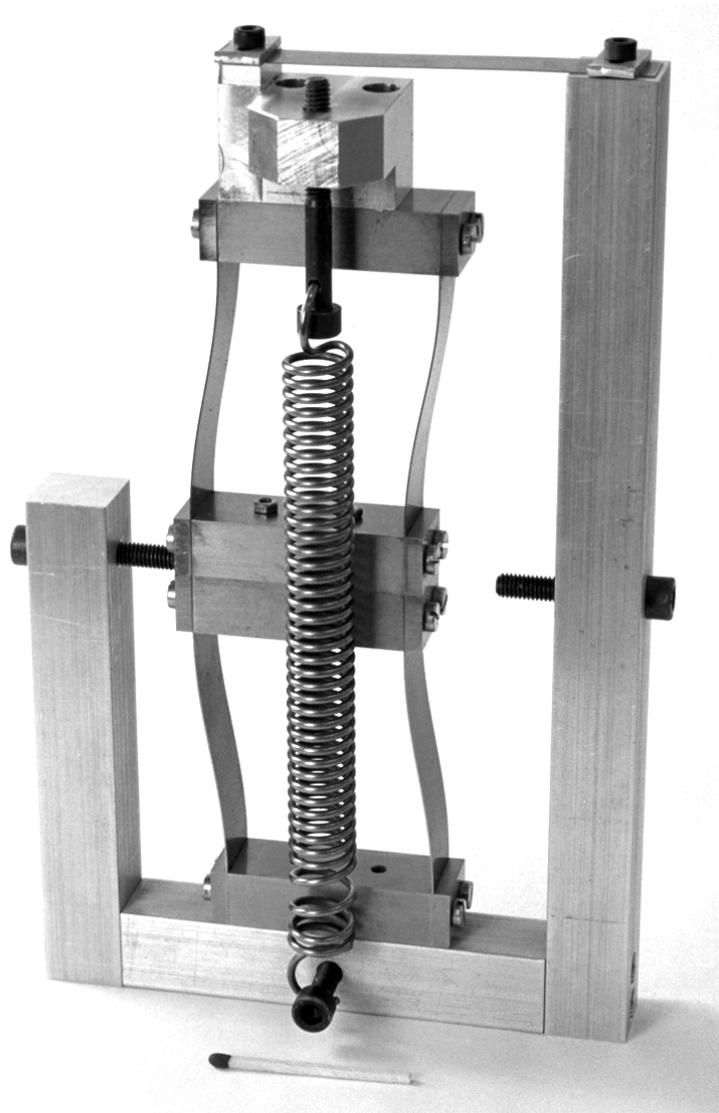
$$K = \frac{N}{\frac{2}{S} \tan \frac{Sl}{2} - l} \quad \text{with } S = \sqrt{\frac{N}{EI}}$$



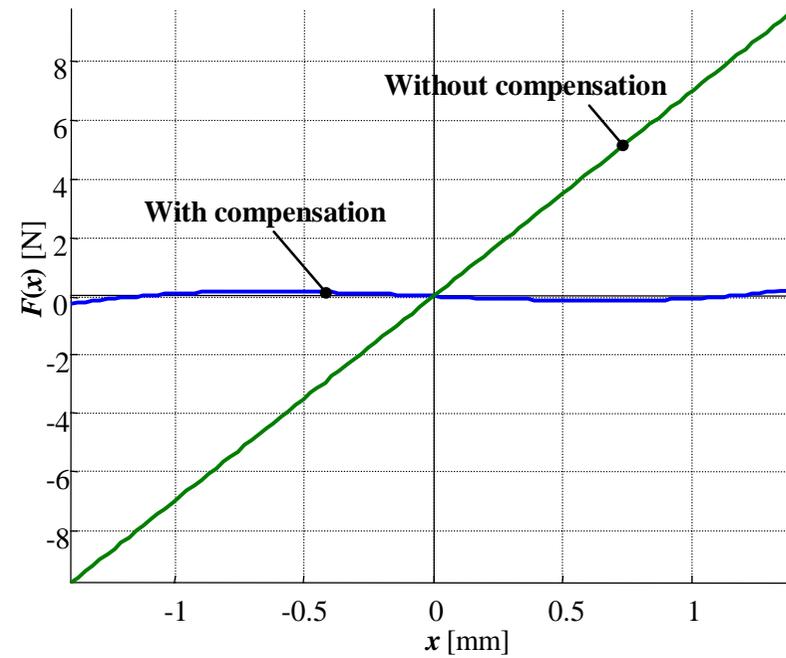
Stiffness K with respect to load N



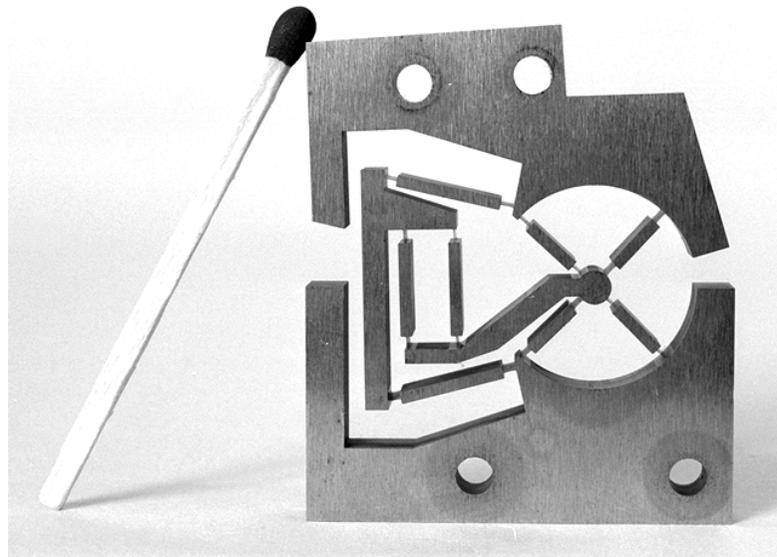
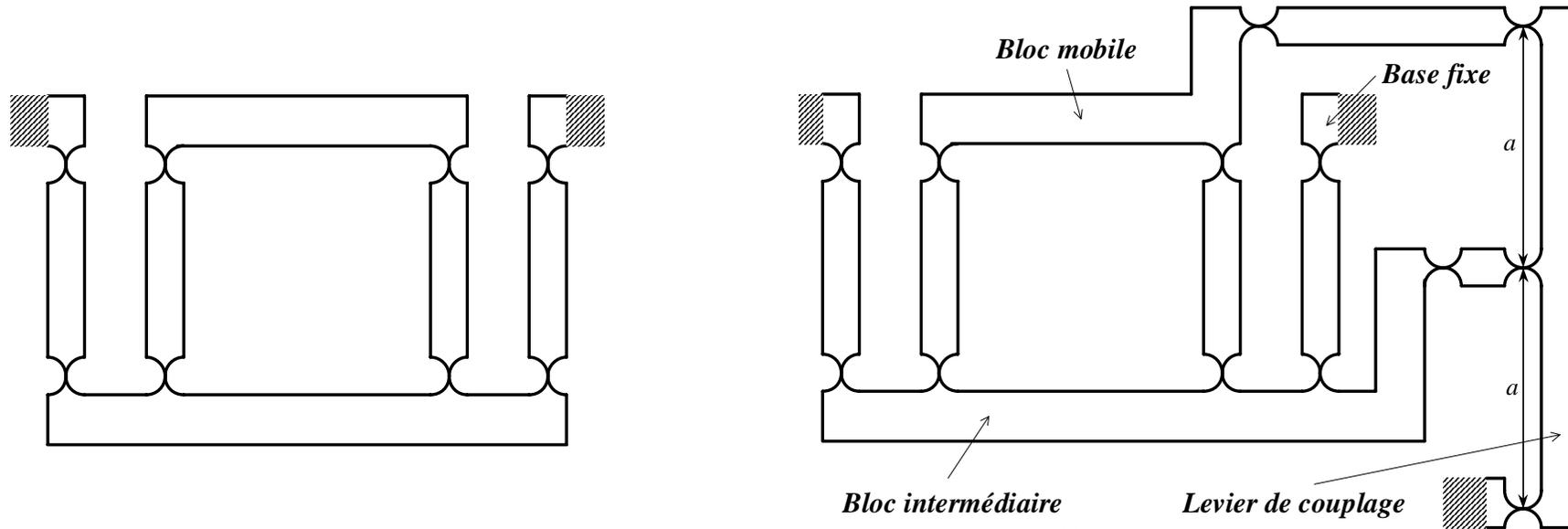
Tuneable stiffness translation bearing



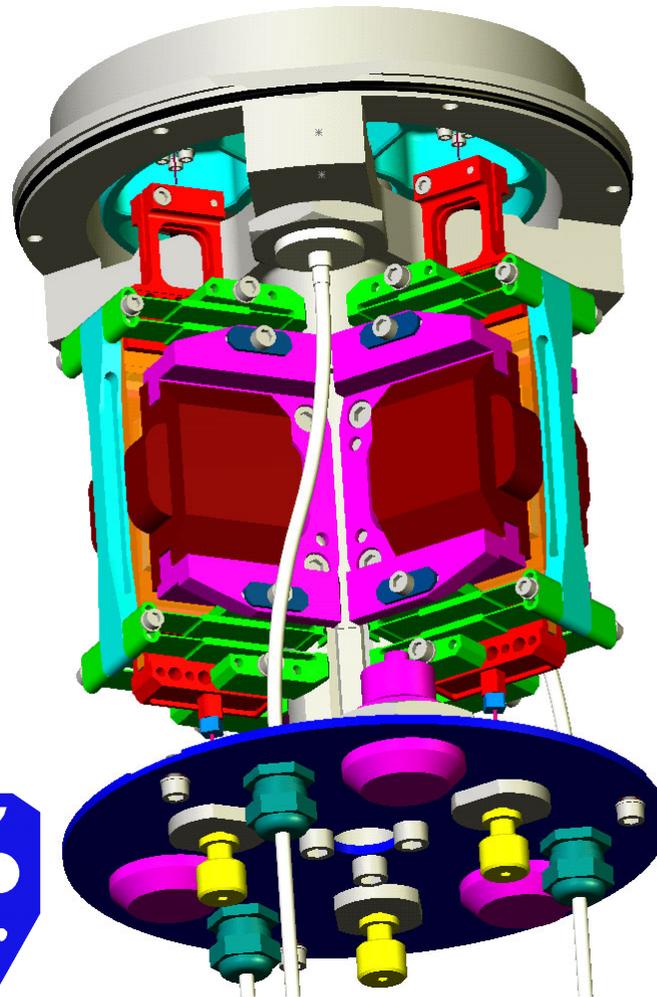
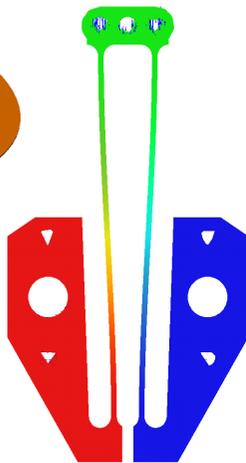
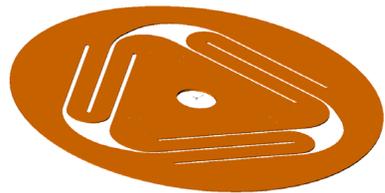
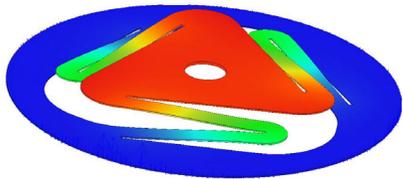
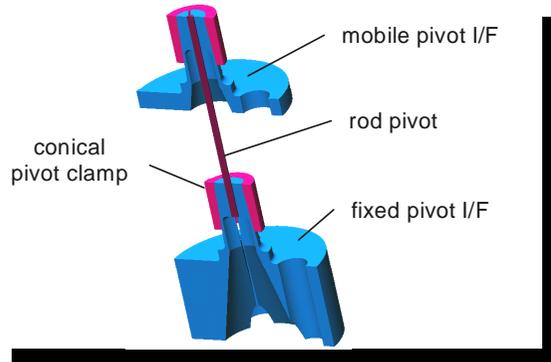
Force-Deformation characteristic



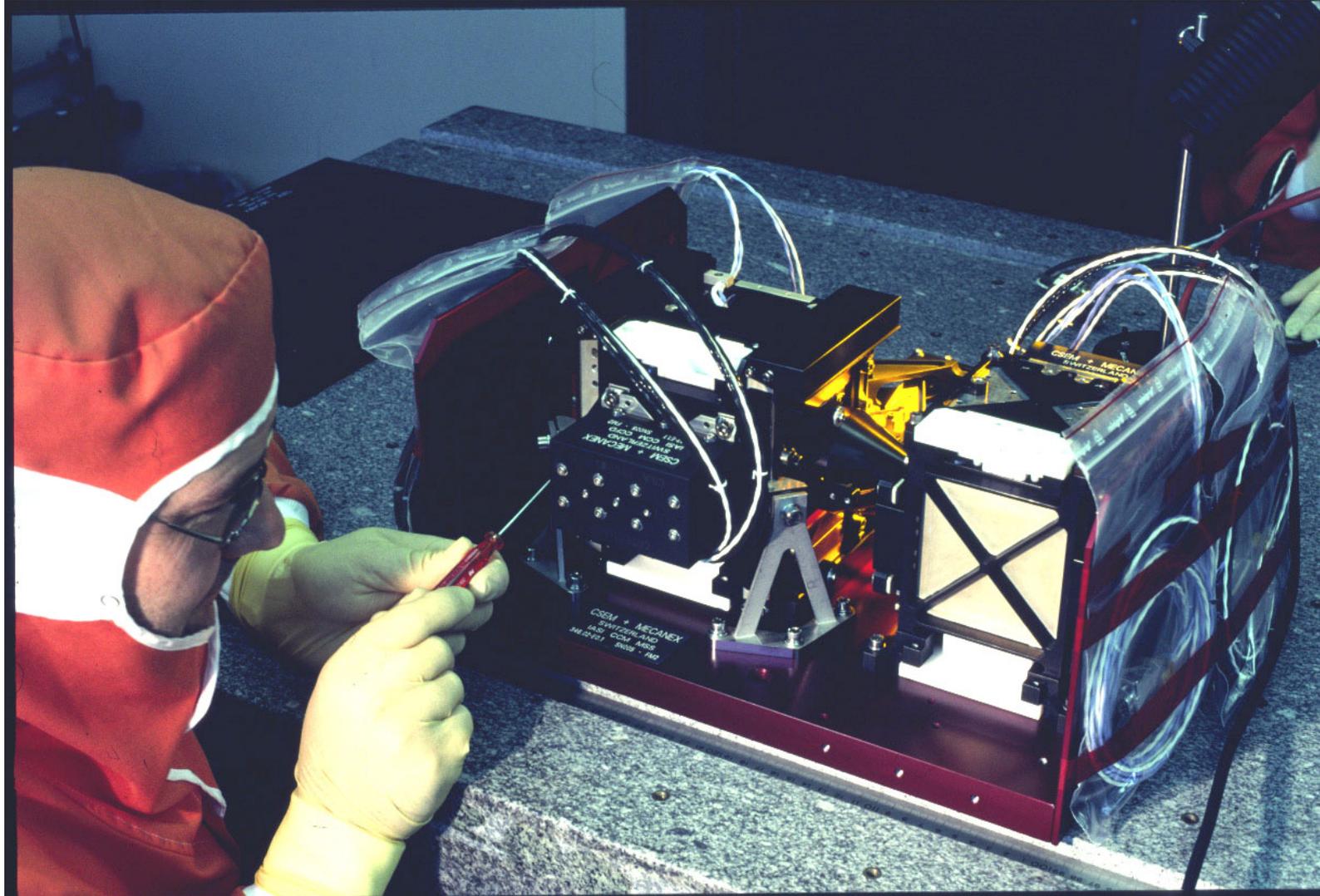
Stroke maximisation and parasitic movement compensation



NAOS flexible structure

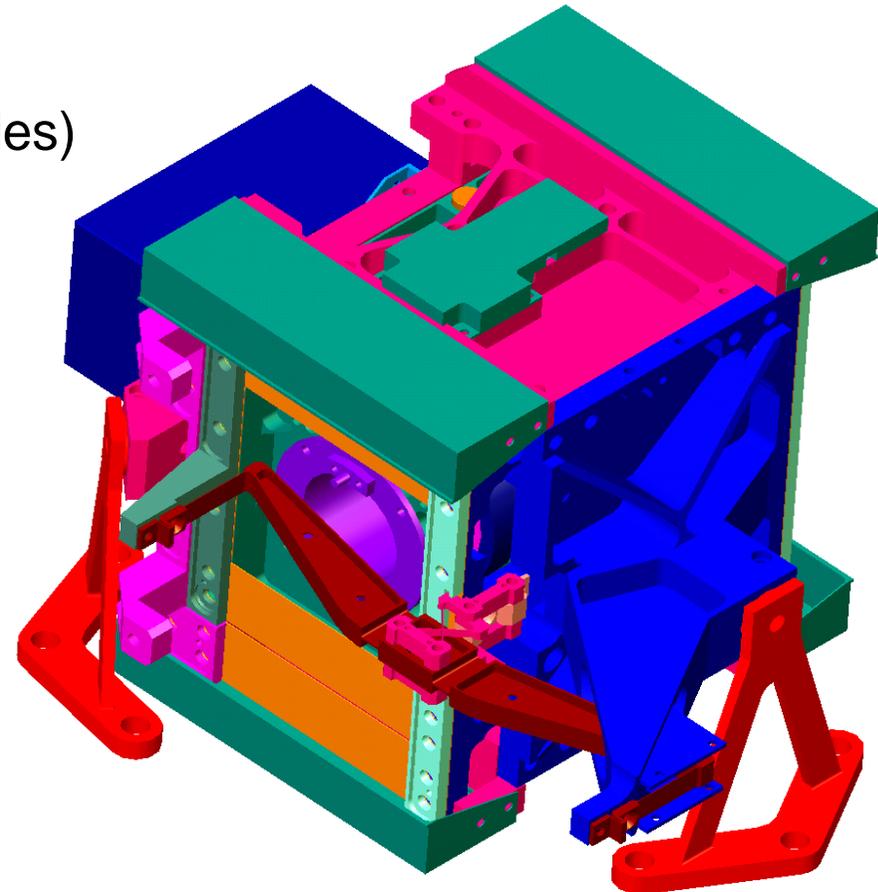


Corner Cube Mechanism for IASI instrument on METOP



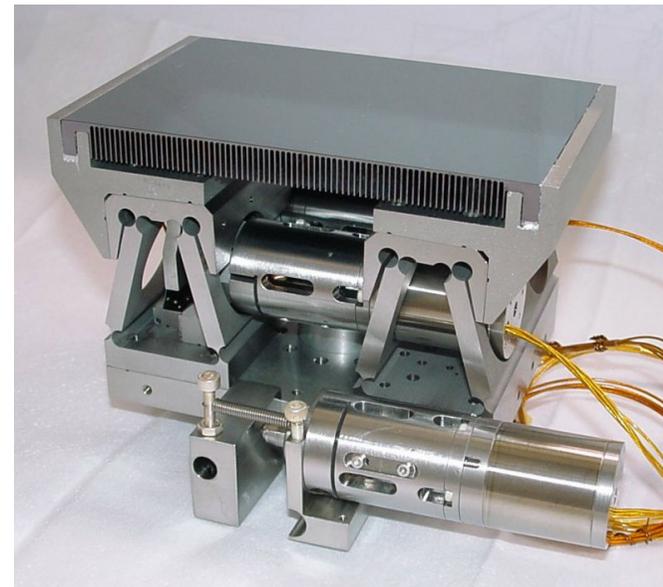
CCM main specifications

- Axial guiding for interferometer linear scanner
- Displacement ± 12 mm
- Lateral error off-axis $<1 \mu\text{m}$
- 2.5 Hz constant velocity travel
- Lifetime : 5 years non-stop ($5 \cdot 10^8$ cycles)



Why compliant mechanisms @ accelerators

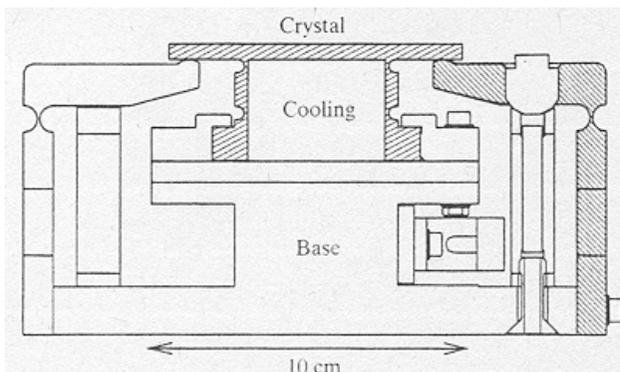
- The technological characteristics of SR and other accelerator facilities pose severe challenges in terms of stability and reproducibility of the beam position => optical elements must be moved with resolutions and accuracies in the nm and μ rad region in an UHV environment with “hostile” characteristics (thermal variations, vibrations, ...)
- Compliant mechanisms offer the high-precision coupled with UHV, radiation and high- or cryo-temperature compatibility
- They are also characterized by simple, reliable and maintenance free design



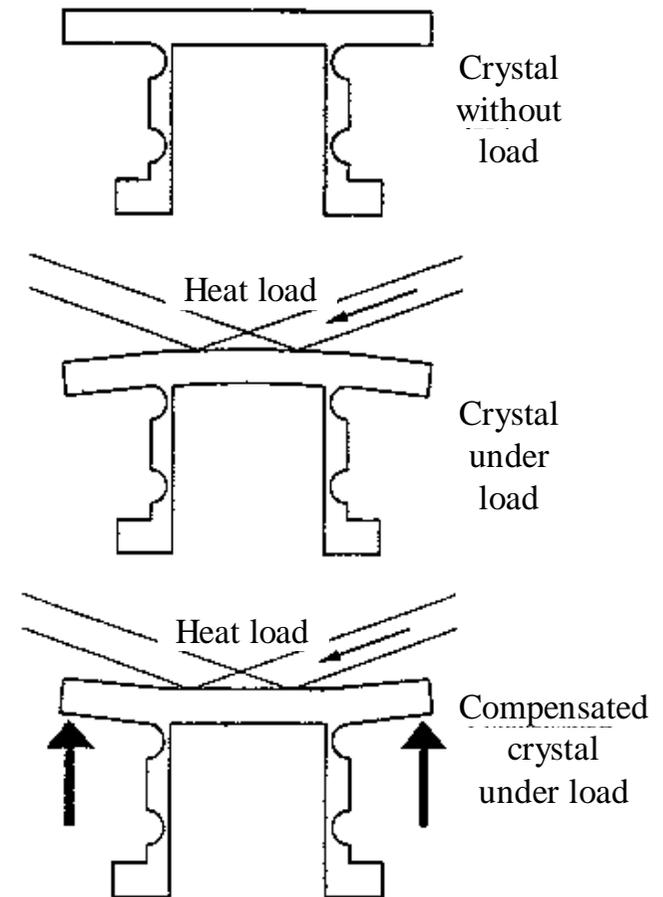
ESRF sagittal bender now commercialised through Oxford Instruments – used also on the SLS Materials Science beamline

Compliant Mechanisms Used @ SLS (1)

High Heat Load Monochromator Crystal Mount – Materials Science Beamline

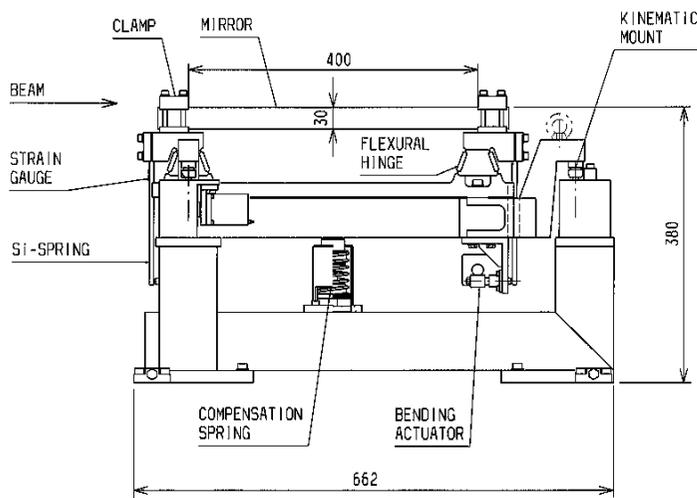
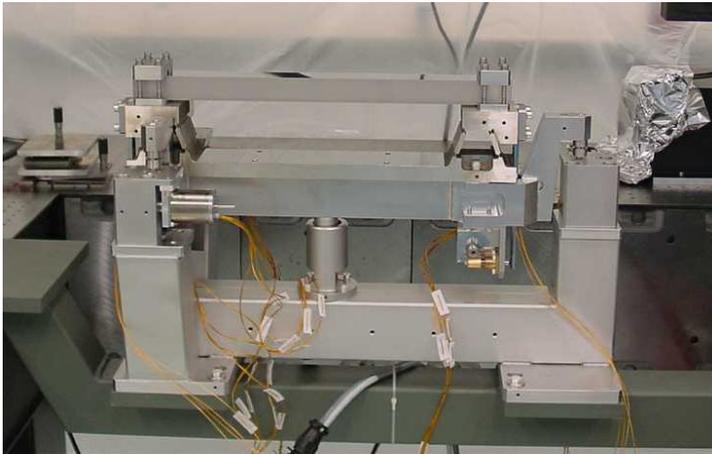


- Collaboration with HASYLAB at DESY, Hamburg (D)
- 1st mono crystal (Si (111)) absorbs up to 1.1 kW of power (up to 3 W/mm²)
- Elastic hinges in crystal feet decouple it from the support structure and allow the adaptation of its shape
- The compensation of the convex bowing of the reflection surface induced by heat load is achieved by loading the crystal “wings”
- The supports of the lever arms comprise again a set of flexural elements used to achieve their longitudinal and transversal compliance



Compliant Mechanisms Used @ SLS (2)

In-Vacuum Dynamic Mirror Bender – Protein Crystallography Beamline



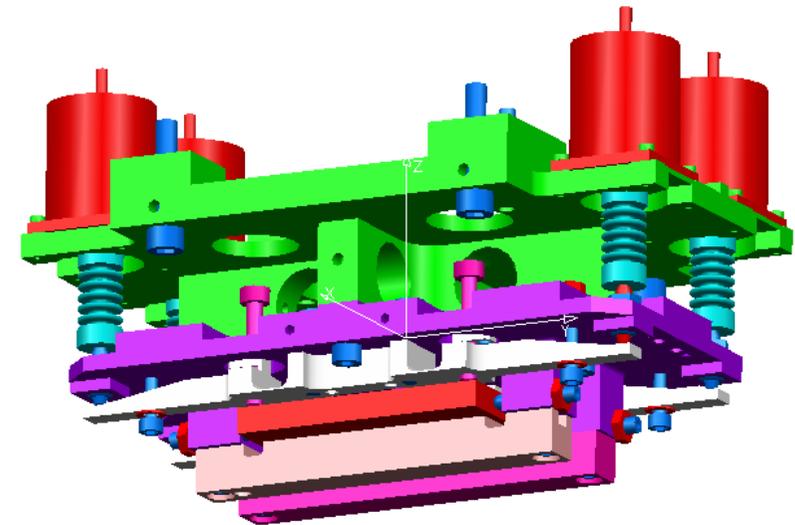
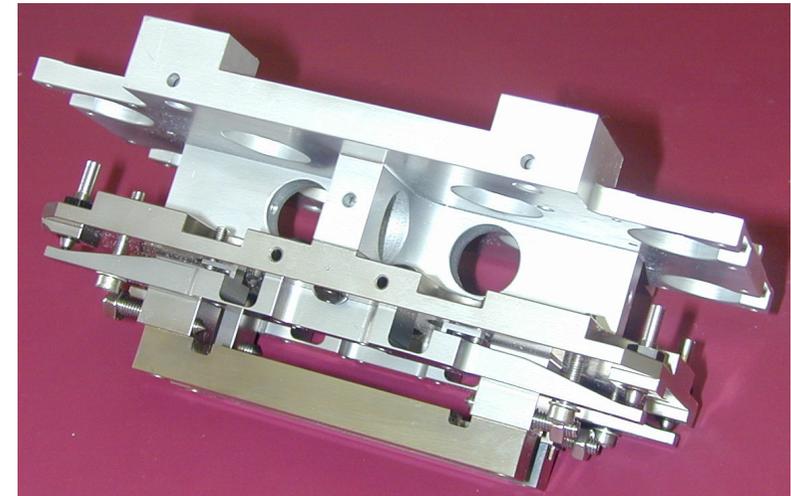
- Collaboration with ESRF, Grenoble (F)
- Vertical focusing rhodium coated fused silica mirror placed on the same optical table and downstream of the double crystal monochromator
- Dynamically bendable providing radiuses of curvature in the 400-12000 m range via 2 independent bending moments at mirror ends through hysteresis-free Si-springs
- The necessary rotational degrees of freedom and the uncoupling of the mirror from its basement are assured through a set of EDM machined flexure hinge based joints
- First experiences show that a sub- μ rad bending reproducibility can be obtained



Compliant Mechanisms Used @ SLS (3)

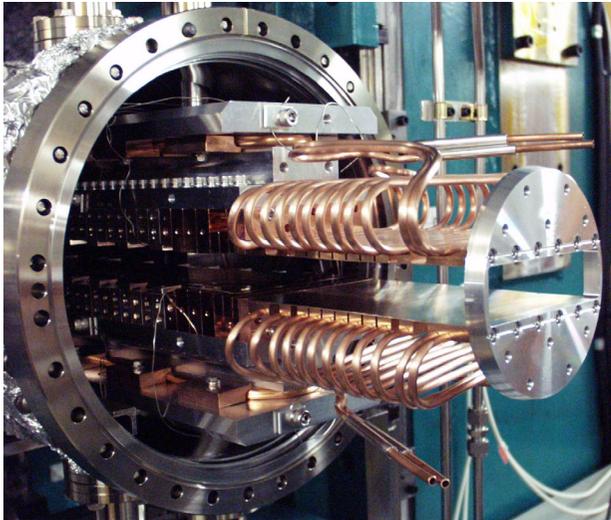
Sagittal Crystal Bender – Protein Crystallography Beamline

- Sagittal focusing of the second monochromator Si (111) crystal
- Provides an elegant way for dynamical micro-focusing of undulator radiation in the horizontal plane
- Bending achieved by means of 4 motorized micrometer screws and elastic elements-based lever arms
- First tests: at 10 keV a 6 mm beam was focused to 20 μm with an efficiency greater than 90%
- Dynamic focusing was also demonstrated
- Together with the vertical focusing bender, the micro-focusing of the beam to the designed values (10 x 25 μm^2), as well as a 0.1 eV energy reproducibility of the monochromator, were reached
- PSI patented

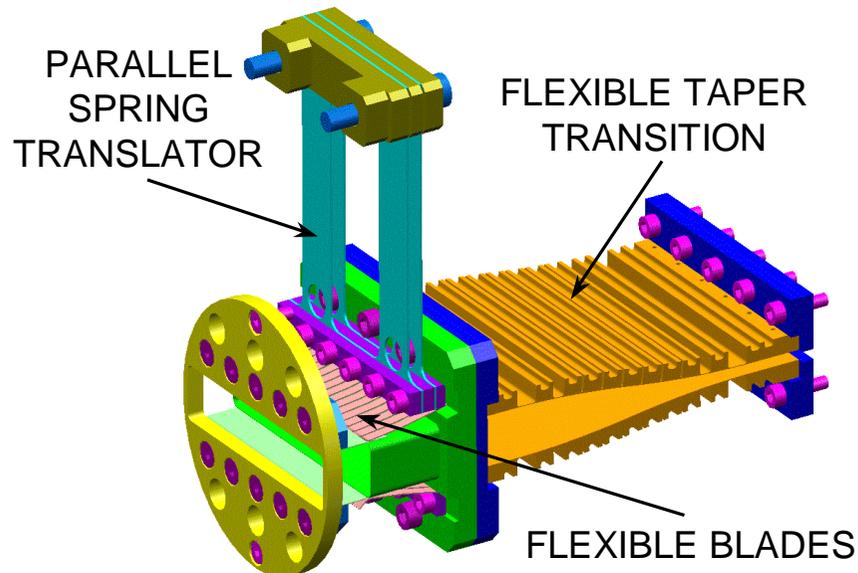


Compliant Mechanisms Used @ SLS (4)

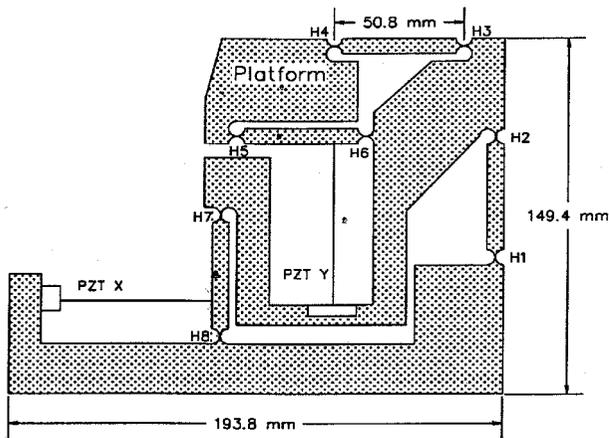
Flexible Taper Transition – In-Vacuum Undulators



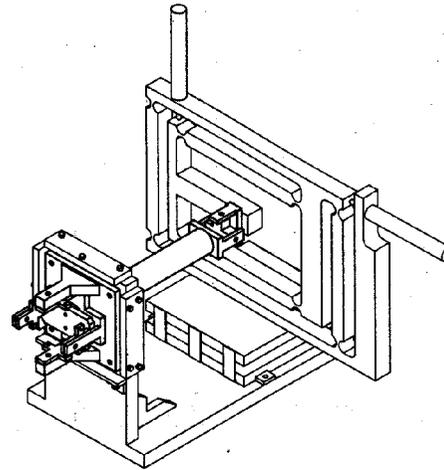
- Collaboration with Spring-8, Japan
- A ribbon cellular CuBe structure provides a smooth transition between the vertical aperture of the adjacent fixed taper section and the in-vacuum magnet carrying beams of the undulator, thus minimizing any impedance discontinuity
- Shape optimized via non-linear FEM analysis to increase fatigue lifetime
- In a further development step longitudinal compliance was assured via a parallel spring translator (+ a flexible-blades based transition) thus avoiding eventual axial-stresses-induced yielding due to the differential thermal expansion of the UHV chamber and the magnet carrying beams during bake-out



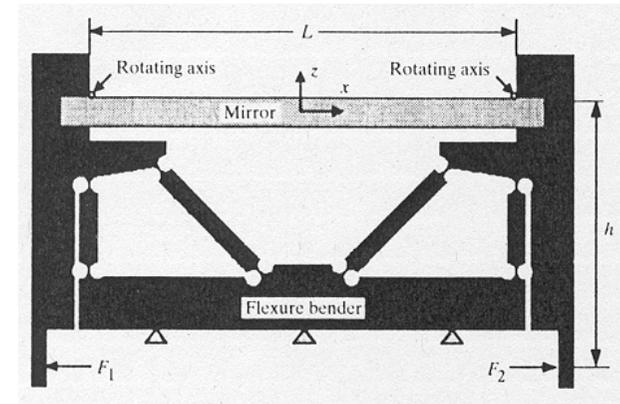
Compliant Mechanisms @ Other SR Facilities



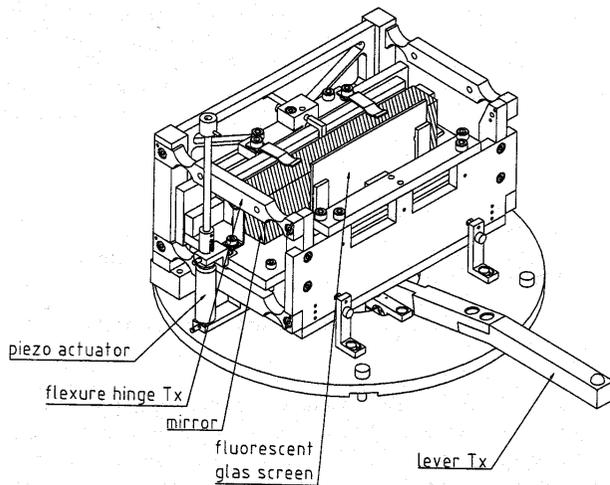
Scanning X-ray microscope micropositioning stage, Wisconsin (USA)



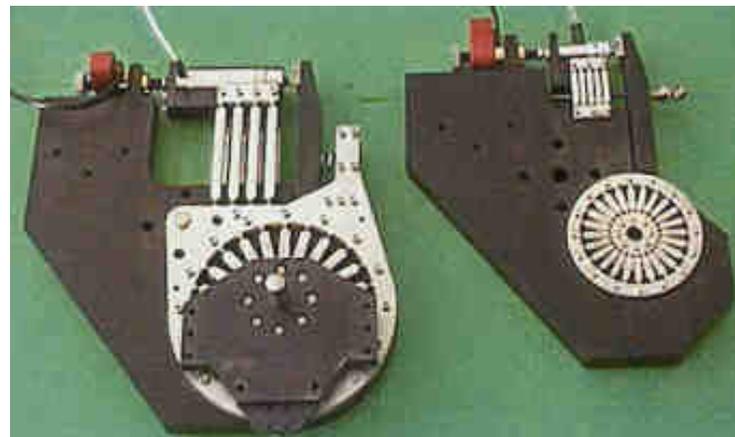
Mirror manipulator, Elettra, Trieste (I)



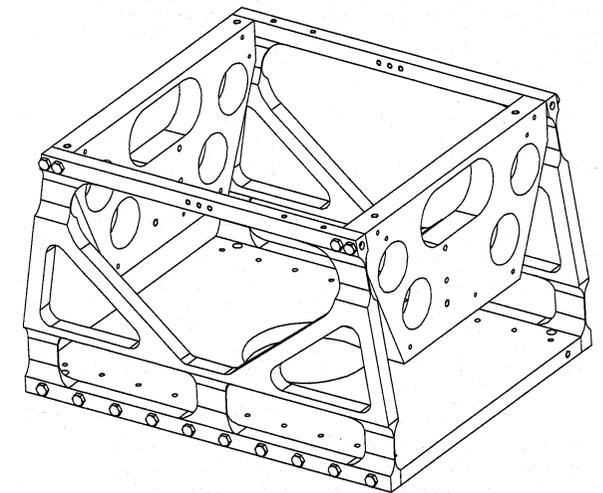
Mirror bender, ESRF, Grenoble (F)



Refocusing mirror holder, Bessy II, Berlin (D)



High-stiffness monochromator weak-link mechanism, APS, Argonne (USA)



Switching mirror flexible parallelogram, Bessy II, Berlin (D)

Conclusion

- Mastering the design of complex flexible structures
- Mastering the interactions at the system level between
 - Mechanical structure
 - Actuators
 - Sensors
 - Electronics
 - Control algorithms

allows to benefit from the compliant mechanisms approach in the design of accelerator equipment and instrumentation.